INC 342 Feedback Control Systems: Lecture 11 Frequency Domain Analysis

Asst. Prof. Dr.-Ing. Sudchai Boonto

Department of Control Systems and Instrumentation Engineering King Mongkut's University of Technology Thonburi





- The most widely used graphical representation of a frequency response is the Bode diagram, developed in the Bell laboratories in the 1930s by W. H. Bode.
- Magnitude and phase are plotted versus frequency in two separate plots, where a log scale is used for magnitude and frequency and a linear scale for the phase.
- The log scale is useful because the transfer function is composed of pole and zero factors which can be added graphically.
- For example

$$G(j\omega) = \frac{g_1(j\omega)g_2(j\omega)}{g_3(j\omega)}$$

Using the notation

$$g_i = |g_i| e^{j\varphi_i}$$

This can be written as

$$G = |G|e^{j\phi} = \frac{|g_1||g_2|}{|g_3|}e^{j(\phi_1 + \phi_2 - \phi_3)}$$

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Thus

$$|G| = \frac{|g_1||g_2|}{|g_3|}, \ \phi = \varphi_1 + \varphi_2 - \varphi_3$$

• the phase of G is the sum of the phase angles of the factors, and on a log scale we also have

$$\log |G| = \log |g_1| + \log |g_2| - \log |g_3|$$

It is standard to measure the logarithmic gain $\log |G|$ in dB, the definition is

 $|G|_{\mathsf{dB}} = 20 \log |G|$

First order term



Second order term



Example



Consider

$$G(s) = \frac{10(s+1)}{s+4}$$

```
s = tf('s');
G = 10*(s+1)/(s+4);
bode(G);
% or
w = logspace(-2,2,200)
% set the frequency range from 10<sup>-2</sup> to 10<sup>2</sup> with 200 sample points
bode(G,w)
```



Delay time reduces the phase margin of the system.

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Bandwidth consider a first-order system

$$G(s) = \frac{b_0}{s+a_0} = \frac{b_0/a_0}{\frac{1}{a_0}s+1} = \frac{K_c}{\tau s+1}$$



Bandwidth of the second order system

$$G(s) = \frac{K}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

We can take

 $\omega_b \approx \omega_n$

as a reasonable approximation of the bandwidth. We also have

$$\omega_b \approx \frac{1.7}{t_r},$$

where t_r is a rise-time of the second order system.

minimum phase system A system with transfer function G(s) is called *minimum phase* if it has no pole or zero on the right half plane

The definition implies that a minimum-phase system is stable; in addition there must be no zeros in the right half plane. Conversely, a system is *non-minimum phase* if it has right half plane zeros or poles or both.

$$G_1(s)=\frac{1}{s+1} \quad \text{stable and minimum-phase}$$

$$G_2(s)=\frac{1}{s-1} \quad \text{unstable and nonminimum-phase}$$



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Bode and Nyquist plot of

$$G(s) = \frac{1}{s+1}$$



The idea of Nyquist plot, we consider the transfer function

$$G(s) = rac{1}{s+1}$$
 or $G(j\omega) = rac{1}{j\omega+1}$

For $\omega=0$ we have G=1 , and for $\omega=\infty$ we have G=0. At the corner frequency $\omega=1$

$$G(j\omega) = \frac{1}{1+j} = \frac{1}{2} - j\frac{1}{2}$$

Actually the magnitude and phase of $G(j\omega)$ can be read from the Bode plot.

- The value of the magnitude are 1 (or 0 dB) or 0 (or $-\infty$ dB) and the phase angles are 0° and -90°
- At the corner frequency, the magnitude is $1/\sqrt{2}$ (-3dB) and the phase is -45° .
- The complex values at the frequencies 0, 1 and ∞ are marked in the G(s)-plane.
- Doing this for sufficiently many frequencies reveals that the points are located on a semicircle centered at 1/2; this semicircular plot is the Nyquist plot of G(s) for positive frequencies.
- The Nyquist plot of negative frequencies is a mirror image of the positive frequencies.

Consider a second order system

$$G(s) = \frac{1}{s(s+1)}$$

Evaluated on the imaginary axis

$$G(j\omega) = \frac{1}{j\omega(j\omega+1)} = \frac{1}{-\omega^2 + j\omega}$$
$$= \frac{-\omega^2 - j\omega}{\omega^4 + \omega^2} = -\frac{1}{\omega^2 + 1} - j\frac{1}{\omega(\omega^2 + 1)}$$

We have

$$\begin{split} \omega &= 0: \qquad G = -1 - j\infty \\ \omega &= 1: \qquad G = -\frac{1}{2} - j\frac{1}{2} \\ \omega &= \infty: \qquad G = 0 \end{split}$$

Bode and Nyquist plot of

$$G(s) = \frac{1}{s(s+1)}$$



The Nyquist stability criterion is based on Cauchy's principle; the idea is to use the contour evaluation o fan open-loop transfer function to determine the presence of unstable closed-loop poles.

Assume we have a transfer function L(s)

$$L(s) = \frac{s - z}{(s - p_1)(s - p_2)}$$



- In the *s*-plane, two poles and a zero are marked, together with a test point *s*₀ which is moved clockwise along a closed contour *C*.
- We are interested in the change of the phase angle of $L(s_0)$ when s_0 is move around the closed contour C.
- The phase angel of $L(s_0)$ is the sum of the zero angel and the negative pole angels indicated inten plot.
- Full traverse, the change of the phase angle is zero.

- The function L(s) maps each point on C into the L(s)-plane, and the point $L(s_0)$ moves along a closed contour which is the mapping of C as s_0 move along C.
- ϕ denotes the phase angle of $L(s_0)$.
- The plot shows that the change of the phase angle of L(s₀) after a full traverse is zero,
 i.e. Δφ = 0°.



- One of poles of L(s) is enclosed by C.
- In this case the phase change of $L(s_0)$ after a full transverse is not zero: the angle of the enclosed pole undergoes a change of 360° . If s_0 moves clockwise, then $L(s_0)$ move counterclockwise and we have $\Delta \phi = 360^{\circ}$.
- This contour must encircle the origin of the L(s)-plane counterclockwise.
- If instead of a pole a zero is enclosed, $\varDelta\phi=-360^\circ$ and $L(s_0)$ encircles the origin clockwise.



- Two poles are enclosed, and we have $\Delta \phi = 720^{\circ}$ after one traverse along C.
- Therefore the mapping of C must encircle the origin of the L(s)-plane two times counterclockwise.

Nyquist's idea was to use this fact to detect the presence of closed-loop poles in the right half plane. For this purpose, the contour C must be chosen such that it encloses the whole right half plane. Such a contour, known as the *Nyquist path*.





The closed-loop characteristic equation is

1 + KL(s) = 0

An unstable zero of 1 + KL(s) indicates an unstable closed-loop pole. For Nyquist plot, instead of evaluating 1 + KL(s) and checking encirclements of the origin, we can equivalently evaluate the open-loop transfer function KL(s) and check encirclements of the point -1



• To evaluate KL(s) along the Nyquist path means to evaluate along the $j\omega$ -axis from $\omega = -\infty$ to $\omega = \infty$, and along the infinite arc.

- However, the transfer functions of physical systems are zero at infinite frequency, and the infinite arc in the *s*-plane is mapped into the origin of the L(s)-plane.
- Therefore, KL(s) needs to be evaluated only from $-j\infty$ to $j\infty$.
- This yields precisely the Nyquist plot of KL(s) for positive and negative frequencies.

- The number of encirclements of the point -1 is not only influenced by the zeros but also by *poles* of 1 + KL(s) in the right half plane.
- If the right half plane contains a zero or a pole of 1 + KL(s), the Nyquist plot of KL(s) encircles the point -1 (clockwise or counterclockwise, respectively).
- To distinguish between poles and zeros of the function $1+\mathit{KL}(s),$ we write $\mathit{L}(s)=\mathit{b}(s)/\mathit{a}(s)$ to obtain

$$1 + KL(s) = \frac{a(s) + Kb(s)}{a(s)}$$

- the zeros of the function 1 + KL(s) are the closed-loop poles, and
- the *poles* of the function 1 + KL(s) are the *open-loop poles* (the poles of L(s))
- If the open loop transfer function is unstable, the number of unstable poles is known.
 So that can be taken into account when checking closed-loop stability.
- If we let Z denote the number of unstable closed-loop pole, and P the number of unstable open-loop poles, then the above considerations show that the Nyquist plot of KL(s) encircles N = Z - P times clockwise the point -1.

Nyquist Stability Test

- 1. Draw the Nyquist plot of KL(s)
- 2. Determine the number N of clockwise encirclements of the point -1 and the number P of unstable open-loop poles
- 3. The closed-loop system has Z = N + P unstable poles.

If the open loop transfer function is stable, then the closed-loop system is stable if the Nyquist polt does not encircle the point -1. If KL(s) has one unstable pole, then closed-loop stability requires one counterclockwise encirclement of -1.

Consider

$$KL(s) = \frac{K}{s+1}$$

- The Nyquist plot is shown in Figure, it is a circle centered at K/2 with radius K/2
- Because P = 0 (no unstable poles of L(s)) and N = 0 (no encirclement of -1) for all K > 0
- The closed-loop system is stable for all positive K.



Consider

$$KL(s) = \frac{K}{s(s+1)}$$



- The Nyquist plot is in fact closed by an arc at infinity.
- The Nyquist path has been modified to avoid the pole at the origin by making an infinitely small detour to the right.

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- It is this small arc that is mapped into an arc at infinity, and to determine whether or not the Nyquist plot encircles the point -1.
- It is important to know whether this infinite arc encloses the right half plane or the left half plant.
- One the small arc, three test points s_i , i = 1, 2, 3 are marked.
- Because the radius of the semicircle around the origin is infinitely small, the magnitude
 of KL(s_i) is infinite, and the phase angles determine by the pole angles are

$$\arg KL(s_1) = +90^\circ, \ \arg KL(s_2) = 0^\circ, \ \arg KL(s_3) = -90^\circ$$

- This shows that the Nyquist plot is completed by aan infinite arc to the right.
- Because the modified Nyquist path does not encircle the pole at the origin, we have P = 0, and from the Figure we conclude that there is no encirclement of -1 for any positive value of K (i.e. N = 0)
- Therefore the closed-loop system is stable for any positive gain.



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Consider the transfer function

$$L(s) = \frac{10}{(s+1)^3} = \frac{10}{s^3 + 3s^2 + 3s + 1}$$

Substituting $j\omega$ for s gives

$$L(j\omega) = \frac{10}{(j\omega)^3 + 3(j\omega)^2 + 3j\omega + 1}$$

At low frequencies $\omega << 1$ we have

$$L \approx 10 \Rightarrow |L| \approx 10, \phi \approx 0^{\circ}$$

and at high frequencies

$$L \approx \frac{10}{(j\omega)^3} = \frac{10}{-j\omega^3} = j\frac{10}{\omega} \implies |L| \approx \frac{10}{\omega^3}, \ \phi \approx -270^\circ$$



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- The left hand side K = 1
- The right hand side K = 0.5
- The Nyquist plot of L(s) encircles the critical point -1 two time clockwise (N = 2). Because L(s) has no unstable pole (P = 0), this implies that the closed-loop system has two unstable poles when K = 1

Gain and Phase Margin

The Nyquist stability test does not only indicate whether a closed-loop system is stable, it also gives information about the "distance" from the stability boundary.

- Such a measure is called a *stability margin*
- The upper bound on *K*, which the closed-loop system becomes unstable, is called the *gain margin* (GM) of the system.
- The phase margin (PM) is defined as the maximum phase change of L(s) that the closed-loop system can tolerate before it becomes unstable.



Gain and Phase Margin



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- 1. Norman S. Nise, "Control Systems Engineering,6th edition, Wiley, 2011
- Gene F. Franklin, J. David Powell, and Abbas Emami-Naeini, "Feedback Control of Dyanmic Systems", 4th edition, Prentice Hall, 2002
- 3. Herbert Werner, "Introduction to Control Systems", Lecture Notes
- 4. Li Qiu and Kemin Zhou, "Introduction to Feedback Control", Prentice Hall, 2010